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(54) **Orthogonal polarized wave branching filter and its manufacturing method**

(57) On a terminal end plane of a circular waveguide, metal columnar blocks and cross shaped branching transforming unit for branching two orthogonal linear polarized waves and transforming from circular TE<sub>11</sub> mode to rectangular TE<sub>10</sub> mode are disposed, and two rectangular waveguides are composed so as to form an angle of 45 degrees to the vertical axis and horizontal axis, that is, symmetrically to the axial center of the circular waveguide, in an electric field direction of first linear polarized wave and an electric field direction of second linear polarized wave.

In this constitution, the orthogonal polarized wave branching filter of microwave band for satellite communications can be reduced in size, and moreover the principal components can be formed integrally by injection molding process.

EP 0 834 953 A1

## Description

### BACKGROUND OF THE INVENTION

The present invention relates to an orthogonal polarized wave branching filter for branching two kinds of linear polarized waves orthogonal to each other in a microwave band used in satellite communications.

Recently, in satellite broadcasting and satellite communications using microwave band, waves having two linear polarized waves orthogonal to each other modulated by individual signals are being used. When receiving modulated signals of two linear polarized waves, the two linear polarized waves must be individually separated. A first example of a conventional orthogonal polarized wave branching filter for this purpose is shown in Fig. 1. This is disclosed in Japanese Utility Model Laid-open No. 62-169503/1987. In Fig. 1, mutually orthogonal two linear polarized waves enter a circular waveguide 101 in a direction of electric field as indicated by reference numerals 107 and 108 from an opening 118. Herein, the electric field 107 parallel to the horizontal axis is supposed to be a first polarized wave, and the electric field 108 parallel to the vertical axis is a second polarized wave. A rectangular waveguide for first polarized wave 105 is provided just above a coupled resonance window 111 so as to be orthogonal to the circular waveguide 101. A rectangular waveguide for second polarized wave 106 is connected smoothly to a terminal end of the circular waveguide 101. A reflector 112 made of a metal material is fixed in tight contact with an inner wall of the circular waveguide 101 so as to be parallel to the coupled resonance window 111 at a specific position in the circular waveguide near the coupled resonance window 111.

In thus constituted conventional orthogonal polarized wave branching filter, of the waves entering the circular waveguide opening 118, the first polarized wave 107 is reflected because its electric field is parallel to the reflector 112, and is not propagated further from the reflector 112, and is guided into the rectangular waveguide 105 through the coupled resonance window 111. On the other hand, the second polarized wave 108 having the electric field vertical to the reflector 112 is propagated up to the terminal end of the circular waveguide without being affected by the coupled resonance window 111 and reflector 112, and is transformed into a rectangular TE<sub>10</sub> mode in the smooth junction (circular-rectangular converting portion) with the rectangular waveguide 106, and is guided into the rectangular waveguide 106.

Fig. 2 shows a second example of a conventional orthogonal polarized wave branching filter. This is disclosed in Japanese Patent Laid-open No. 2-29001/1990. In Fig. 2, from an opening 119 of a square waveguide 113 having one end short-circuited, mutually orthogonal two linear polarized waves enter in a direction of electric field as indicated by reference numerals

107 and 108. Herein, the wave 107 having a direction of electric field parallel to the horizontal axis is supposed to be a first polarized wave, and the wave 108 having a direction of electric field parallel to the vertical axis is a second polarized wave. Rectangular waveguides 115, 116 are provided at one side of the square waveguide 113 so as to be parallel to each other through a coupled resonance window. A plurality of conductor plates 114 are provided in the square waveguide 113 near the middle point of the rectangular waveguides 115, 116 so as to be parallel to the vertical axis. A 90-degree phase plate 117 is composed of a dielectric of specific shape and dielectric constant, and is provided in contact with a short-circuit end 120 of the square waveguide 113 to as to form 45 degrees to the vertical axis and horizontal axis. It works as a polarization rotation reflector for rotating the plane of polarization by 90 degrees.

When the first polarized wave 107 and second polarized wave 108 enter from the opening 119 of the square waveguide 113, the first polarized wave 107 is directed to the short-circuit end 120 of the square waveguide 113 without being affected by the conductor plate 114, and is reflected and rotated of the plane of polarization by the 90-degree phase plate 117 which is a polarized wave rotation reflector to become second polarized wave 108, which is directed toward the opening 119, but is reflected by the conductor plate 114 and is entirely sent out to the rectangular waveguide 115. On the other hand, the second polarized wave 108 is reflected by the conductor plate 114, and is not propagated up to the short-circuit end 120 of the square waveguide 113, but is entirely sent out to the rectangular waveguide 116.

In such conventional constitution, however, since the two rectangular waveguides 115, 116 are installed at different distances from the opening 119, the overall length of the orthogonal polarized wave branching filter is long as a matter of course. Besides, it is necessary to install the reflector (conductor plate) 114 and 90-degree phase plate 117, and it is impossible to form integrally by using injection molding means. Accordingly, in mass production, the number of parts and processes increase, and it is hard to assure stable performance due to mounting error.

### SUMMARY OF THE INVENTION

To solve the problems of the prior art, hence, it is an object of the invention to present an orthogonal polarized wave branching filter reduced in the number of parts by eliminating the hitherto required reflector (conductor plate) and 90-degree phase plate, stable in performance by eliminating the mounting process, and small in size, high in performance, and formable by injection molding by disposing the rectangular waveguides at equal distance from the opening.

To achieve the object, a basic constitution of an orthogonal polarized wave branching filter of the inven-

tion comprises a circular waveguide having a terminal end for transmitting a first linear polarized wave and a second linear polarized wave orthogonal to the first linear polarized wave, first and second rectangular waveguides connected from the terminal end of the circular waveguide in the direction of each electric field direction of the first and second linear polarized waves, and a branching transforming unit made of a metal material in a cross form provided in the terminal end plane of the circular waveguide with the longitudinal direction parallel to the direction of each electric field of the first and second linear polarized waves about the axial center of the circular waveguide.

The first and second rectangular waveguides are deflected in halving directions of electric field directions of the first and second linear polarized waves after branching at the terminal end of the circular waveguide to be parallel to each other, with the opening surfaces on a same plane, and current is supplied from the same plane.

In this constitution, two orthogonal polarized waves can be produced at positions at equal distance from the opening of the circular waveguide, so that the entire size of the branching filter can be reduced.

As the means for transforming the transmission mode in the circular waveguide and in the rectangular waveguide efficiently between the circular TE<sub>11</sub> mode and rectangular TE<sub>10</sub> mode, the rectangular waveguide side of the cross shaped branching transforming unit is formed in stairs.

Moreover, by forming a metal columnar block in plural stairs becoming smaller in diameter as going remoter from the terminal end of the circular waveguide in the middle of the cross shaped branching transforming unit, in a shape overlaid on the axial center of the circular waveguide, undesired wave leak between the first and second rectangular waveguides may be prevented.

Incidentally, the operation is unchanged if the circular waveguide of this basic constitution is replaced by a square wave guide having two sides each parallel in the electric field direction of each linear polarized wave, and the partial constitution added to this basic constitution also acts same as above.

In these constitutions, by forming the circular waveguide or square waveguide in a taper shape expanding wider from the terminal end to the opening, forming the cross shaped branching transforming unit and, if necessary, the metal columnar block in plural stairs in a taper shape reducing narrower from the terminal end to the opening, and forming the rectangular waveguide in a taper shape expanding wider toward the opening, it is possible to form integrally by injection molding means, and therefore the number of parts and processes can be curtailed, the production cost is reduced, fluctuations of performance and deterioration due to mounting error can be prevented, and the performance stability and productivity improvement in mass production are outstanding.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a perspective view of an orthogonal polarized wave branching filter in a first prior art.

Fig. 2 is a perspective view of an orthogonal polarized wave branching filter in a second prior art.

Fig. 3 is a front view of an orthogonal polarized wave branching filter in an embodiment of the invention.

Fig. 4 is a plan view of an orthogonal polarized wave branching filter in an embodiment of the invention.

Fig. 5 is a sectional view along cut line S1-S1 of Fig. 3.

#### EMBODIMENTS

Referring now to the drawings, an embodiment of the invention is described below.

Fig. 3 is a front view of an orthogonal polarized wave branching filter in an embodiment of the invention.

The longitudinal direction of a branching transforming unit 2 is disposed at a terminal end plane 1a of a terminal end portion of a taper shaped circular waveguide 1 opened in the direction of an opening 1b, in a direction at an angle of 45 degrees to the vertical axis and horizontal axis. That is, the longitudinal direction of the branching transforming unit 2 is disposed so as to coincide with an electric field direction 7 of a first linear polarized wave of the circular waveguide 1 and an electric field direction 8 of a second linear polarized wave, so as to be formed in a cross shape.

Closely to the terminal end plane 1a of the terminal end portion of the circular waveguide 1, an opening 5a of a rectangular waveguide 5 is disposed in the direction of the electric field direction 7 of the first linear polarized wave, and similarly closely to the terminal end plane 1a of the terminal end portion of the circular waveguide 1, an opening 6a of a rectangular waveguide 6 is disposed in the direction of the electric field direction 8 of the second linear polarized wave.

A three-stair portion 3 of the cross shaped branching transforming unit 2 is disposed at the rectangular waveguide 5, 6 side.

The rectangular waveguides 5, 6 for first and second linear polarized waves are deflected at specified positions, and are installed so that the individual opening surfaces 5b, 6b may be parallel to the horizontal shaft, that is, each central axis may be parallel to the bisector direction of the electric field direction 7 of the first linear polarized wave and the electric field direction 8 of the second linear polarized wave, or in the vertical axis direction.

Fig. 4 is a plan view of an embodiment of the invention. Metal columnar blocks 4 differing in diameter in three stages are overlaid on the axial center of the circular waveguide in the center of the cross shaped branching transforming unit 2. Fig. 5 is a sectional view of Fig. 3 cut along line S1-S1 at an angle of 45 degrees to the vertical axis.

A base portion 3a is formed slightly lower than the stairs 3, and this portion is provided for impedance matching.

The operation of the orthogonal polarized wave branching filter of the embodiment of the invention thus constituted is described below while referring to the drawings.

The TE<sub>11</sub> mode of the circular waveguide and TE<sub>10</sub> mode of the rectangular waveguide can be easily transformed because they are nearly same in electromagnetic field distribution. As shown in Fig. 1, by gradually deforming the circular waveguide into a rectangular waveguide, or, to the contrary, by gradually transforming the rectangular waveguide into a circular waveguide, the modes can be transformed.

In the case of this embodiment, since the rectangular waveguides 5, 6 are connected at right angle to the circular waveguide 1, the method as shown in Fig. 1 cannot be employed. Instead, the modes are transformed by making use of the nature that the both modes are similar.

In the case of circular waveguide, the electromagnetic field distribution is dense in the center and sparse at the ends. In the center, moreover, the electromagnetic field distribution is almost same as in the rectangular waveguide. That is, in the case of circular waveguide, it is necessary to consider only the electromagnetic field distribution near the center, and considering near the center, the TE<sub>11</sub> mode of the circular waveguide and TE<sub>10</sub> mode of rectangular waveguide may be regarded identical. Accordingly, in the stairs 3 of the embodiment, by properly selecting the height of each stair as shown in Fig. 5, coupling of electromagnetic fields occurs between the seam of the circular waveguide 1 and rectangular waveguide 5 or 6 and the flat plane of the stairs 3, and the electromagnetic field is gradually bent, finally bending 90 degrees. This ends bending of electromagnetic field, and also terminates the mode transformation.

Transformation from the rectangular waveguide 5 or 6 side is also the same. By feeding current in the rectangular TE<sub>10</sub> mode 9 from the rectangular waveguide 5 side as shown in the diagram, it is efficiently transformed into the circular TE<sub>11</sub> mode 10 by the stairs 3 of the cross shaped branching transforming unit 2, thereby appearing in the opening plane 1b of the circular waveguide 1.

At this time, by the effect of the metal columnar blocks 4, the wave is not coupled with the rectangular waveguide 6, and the wave supplied from the rectangular waveguide 5 completely appears on the opening plane 1b of the circular waveguide 1.

This reason is explained. In Fig. 3, suppose only the first polarized wave of electric field direction 7 enters from the circular waveguide 1. If metal columnar blocks 4 are not provided, the electric field spreads and propagates in the entire circular waveguide 1, and is partly coupled with the rectangular waveguide 6 for second

5 polarized wave and propagates, and therefore it is sent out to the opening plane of the rectangular waveguide 6 for second polarized wave in which it is not supposed to appear in principle. By contrast, when the metal columnar blocks 4 are provided, since the electric field is present between the inner wall of the columnar waveguide 1 near the rectangular waveguide 5 for first polarized wave and the metal columnar blocks 4, the electric field 7 of first polarized wave is not present near the rectangular waveguide 6 for second polarized wave, and hence it will not be coupled with the rectangular waveguide 6 for second polarized wave. Therefore, all of the first polarized wave 7 is issued from the rectangular polarized wave 5 for first polarized wave.

10 Similarly, in the case of entrance in rectangular TE<sub>10</sub> mode from the rectangular waveguide 5 for first polarized wave, the electric field transformed into TE<sub>11</sub> mode of the circular waveguide by the stairs 3 similarly propagates between the inner wall at the rectangular waveguide 5 side for first polarized wave and the metal columnar blocks 4, and hence will not be coupled with the rectangular waveguide 6 for second polarized wave. That is, the metal columnar blocks 4 play a role to limit the spreading of electric field.

15 The wave appearing on the opening plane 1b of the circular waveguide 1 is a first linear polarized wave of electric field direction 7 as shown in Fig. 3. Similarly, by feeding current from the rectangular waveguide 6, all supplied waves are transformed in mode and sent out to the opening plane 1b of the circular waveguide 1. At this time, the wave is changed to the second linear polarized wave of electric field direction 8 as shown in Fig. 3. At this time, the opposite side portion to the waveguides 5, 6 with respect to the central axis of the cross shaped branching transforming unit 2 plays the role of impedance matching of waveguides 5, 6 and circular waveguide 1.

20 To the contrary, in Fig. 3, when the first and second linear polarized waves of electric field directions 7 and 8 are entered from the opening plane 1b of the circular waveguide 1, they are branched efficiently by the plural stages of metal columnar blocks 4, and all of the first polarized wave in the electric field direction 7 is sent out from the rectangular waveguide 5, and all of the second polarized wave in the electric field direction 8 is sent out from the rectangular waveguide 6.

25 As clear from Fig. 3, the inside of the circular waveguide 1 is in a taper form expanding widely to the nearer side in the axial direction, and the cross shaped branching transforming unit 2 and metal columnar blocks 4 are in a taper form narrower toward the nearer side in the axial direction. The rectangular waveguides 5, 6 are in a taper form expanding wider toward the upward direction. Thus, the circular waveguide 1, rectangular waveguides 5, 6, cross shaped branching transforming unit 2 including stairs 3, and metal columnar blocks 4 can be formed integrally by manufacturing method of injection molding, by disposing a slid cor to

be inserted from before in the drawing into a die opening in the vertical direction in fig. 3 and of which upper side is a male pattern. As molding material, aluminum, for example, is preferred. Alternatively, only the cross shaped branching transforming unit 2 and metal columnar blocks 4 may be manufactured from other parts by cutting or other method, and attached to the formed main body by press fitting, screw fixing or the like after molding. The stairs 3 and metal columnar blocks 4 are both in three stages, but, they may be also formed in two or four stages as required, and the detail of number or dimension is not particularly limited.

The circular waveguide may be replaced by a square waveguide in which two orthogonal linear polarized waves can be used. When replaced with a square waveguide having two sides parallel to the S1-S1 section in Fig. 3, that is, parallel to the electric field direction 7 of the first linear polarized wave, and two sides parallel to the electric field direction 8 of the second linear polarized wave, it is easy to understand that the same action as explained by reference to Fig. 3 to Fig. 5 may be obtained.

Thus, according to the invention, in the orthogonal polarized wave branching filter, the entire size of the branching filter can be reduced by sending out two orthogonal polarized waves at positions at equal distance from the opening of the circular waveguide.

Moreover, by disposing the metal columnar blocks and cross shaped branching transforming unit for branching two orthogonal polarized waves on the terminal end plane of the terminal end portion of the circular waveguide, forming the circular waveguide, metal columnar blocks, cross shaped branching transforming unit, and rectangular waveguide in a taper form, and forming the entire branching filter integrally by injection molding process, not only the manufacturing and mounting steps of the hitherto required reflector (conductor plate) and 90-degree phase plate can be omitted, but also performance fluctuations and adjusting process due to mounting error in mass production can be eliminated, so that stable performance and notable enhancement of productivity may be presented.

The invention may be embodied in several forms without departing from the spirit of essential characteristics thereof. For example, the circular waveguide may be replaced by the square waveguide having sides in the electric field direction of first polarized wave and electric field direction of second polarized wave as shown in Fig. 2. Therefore, the present embodiments are therefore illustrative and not restrictive, since the scope of the invention is defined by the appended claims rather than by the description preceding them, and all changes that fall within metes and bounds of the claims, or equivalence of such metes and bounds thereof are therefore intended to be embraced by the claims.

## Claims

1. An orthogonal polarized wave branching filter comprising:  
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a circular waveguide having a terminal end for transmitting a first linear polarized wave and a second linear polarized wave orthogonal to the first linear polarized wave,  
first and second rectangular waveguides connected from the terminal end of the circular waveguide in the direction of each electric field direction of the first and second linear polarized waves, and  
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a branching transforming unit made of a metal material in a cross form provided in the terminal end plane of the circular waveguide with the longitudinal direction parallel to the direction of each electric field of the first and second linear polarized waves about the axial center of the circular waveguide.
2. An orthogonal polarized wave branching filter of claim 1, wherein the first and second rectangular waveguides are deflected in halving directions of electric field directions of the first and second linear polarized waves after branching at the terminal end of the circular waveguide to be parallel to each other, with the opening surfaces on a same plane, and current is supplied from the same plane.  
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3. An orthogonal polarized wave branching filter of claim 1, wherein the rectangular waveguide side of the cross shaped branching transforming unit is formed in stairs.  
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4. An orthogonal polarized wave branching filter of claim 1, wherein metal columnar blocks in plural stages becoming smaller in diameter as going remoter from the terminal end of the circular waveguide are overlaid in the center of the cross shaped branching transforming unit, on the axial center of the circular waveguide.  
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5. An orthogonal polarized wave branching filter comprising:  
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a square waveguide having a terminal end for transmitting a first linear polarized wave and a second linear polarized wave orthogonal to the first linear polarized wave,  
first and second rectangular waveguides connected from the terminal end of the square waveguide in the direction of each electric field direction of the first and second linear polarized waves, and  
55  
a branching transforming unit made of a metal material in a cross form provided in the termi-

- nal end plane of the square waveguide with the longitudinal direction parallel to the direction of each electric field of the first and second linear polarized waves about the axial center of the square waveguide. 5
6. An orthogonal polarized wave branching filter of claim 5, wherein the first and second rectangular waveguides are deflected in halving directions of electric field directions of the first and second linear polarized waves after branching at the terminal end of the square waveguide to be parallel to each other, with the opening surfaces on a same plane, and current is supplied from the same plane. 10
7. An orthogonal polarized wave branching filter of claim 5, wherein the rectangular waveguide side of the cross shaped branching transforming unit is formed in stairs. 15
8. An orthogonal polarized wave branching filter of claim 5, wherein metal columnar blocks in plural stages becoming smaller in diameter as going remoter from the terminal end of the square waveguide are overlaid in the center of the cross shaped branching transforming unit, on the axial center of the square waveguide. 20
9. A manufacturing method of an orthogonal polarized wave branching filter characterized by forming, in the orthogonal polarized wave branching filter in claim 2, the circular waveguide in a taper form expanding wider from the terminal end portion toward the opening portion, the cross shaped branching transforming unit in a taper form becoming narrower from the terminal end portion toward the opening portion, and the rectangular waveguide in a taper form expanding wider toward the opening portion, and forming integrally by injection molding means. 25
10. A manufacturing method of an orthogonal polarized wave branching filter of claim 9, wherein metal columnar blocks in plural stages becoming smaller in diameter as going remoter from the terminal end of the circular waveguide are overlaid in the center of the cross shaped branching transforming unit, on the axial center of the circular waveguide, in a taper form becoming narrower toward the opening portion of the circular waveguide. 30
11. A manufacturing method of an orthogonal polarized wave branching filter of claim 10, wherein the cross shaped branching transforming unit and metal columnar blocks in plural stages are fabricated from other metal parts, and are attached to the terminal end plane of the terminal end portion of the circular waveguide. 35
12. A manufacturing method of an orthogonal polarized wave branching filter characterized by forming, in the orthogonal polarized wave branching filter in claim 6, the square waveguide in a taper form expanding wider from the terminal end portion toward the opening portion, the cross shaped branching transforming unit in a taper form becoming narrower from the terminal end portion toward the opening portion, and the rectangular waveguide in a taper form expanding wider toward the opening portion, and forming integrally by injection molding means. 40
13. A manufacturing method of an orthogonal polarized wave branching filter of claim 12, wherein metal columnar blocks in plural stages becoming smaller in diameter as going remoter from the terminal end of the square waveguide are overlaid in the center of the cross shaped branching transforming unit, on the axial center of the square waveguide, in a taper form becoming narrower toward the opening portion of the circular waveguide. 45
14. A manufacturing method of an orthogonal polarized wave branching filter of claim 12, wherein the cross shaped branching transforming unit and metal columnar blocks in plural stages are fabricated from other metal parts, and are attached to the terminal end plane of the terminal end portion of the square waveguide. 50
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Fig. 1

PRIOR ART

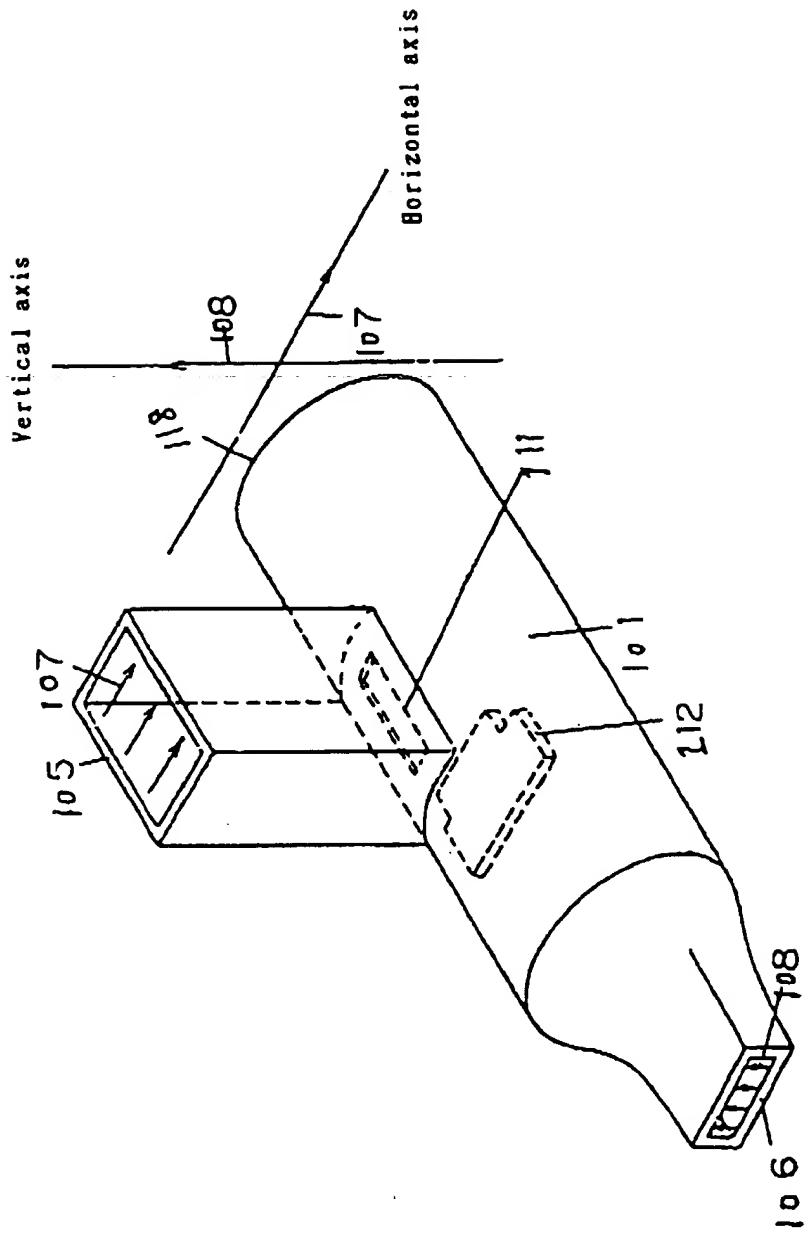


Fig. 2

PRIOR ART

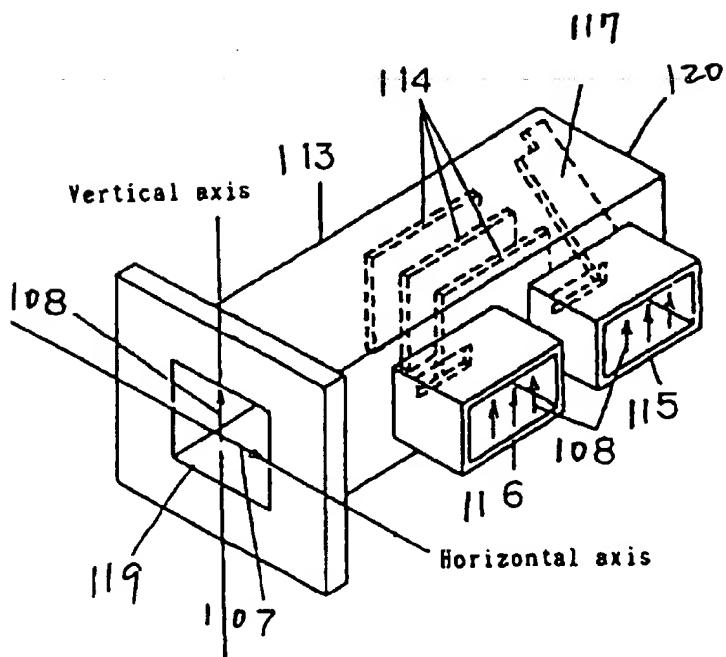


Fig. 3

- 1 Circular waveguide
- 2 Cross shaped branching transforming unit
- 3 Stairs
- 4 Metal columnar blocks
- 5 Rectangular waveguide for first polarized wave
- 6 Rectangular waveguide for second polarized wave
- 7 Electric field direction of first linear polarized wave
- 8 Electric field direction of second linear polarized wave

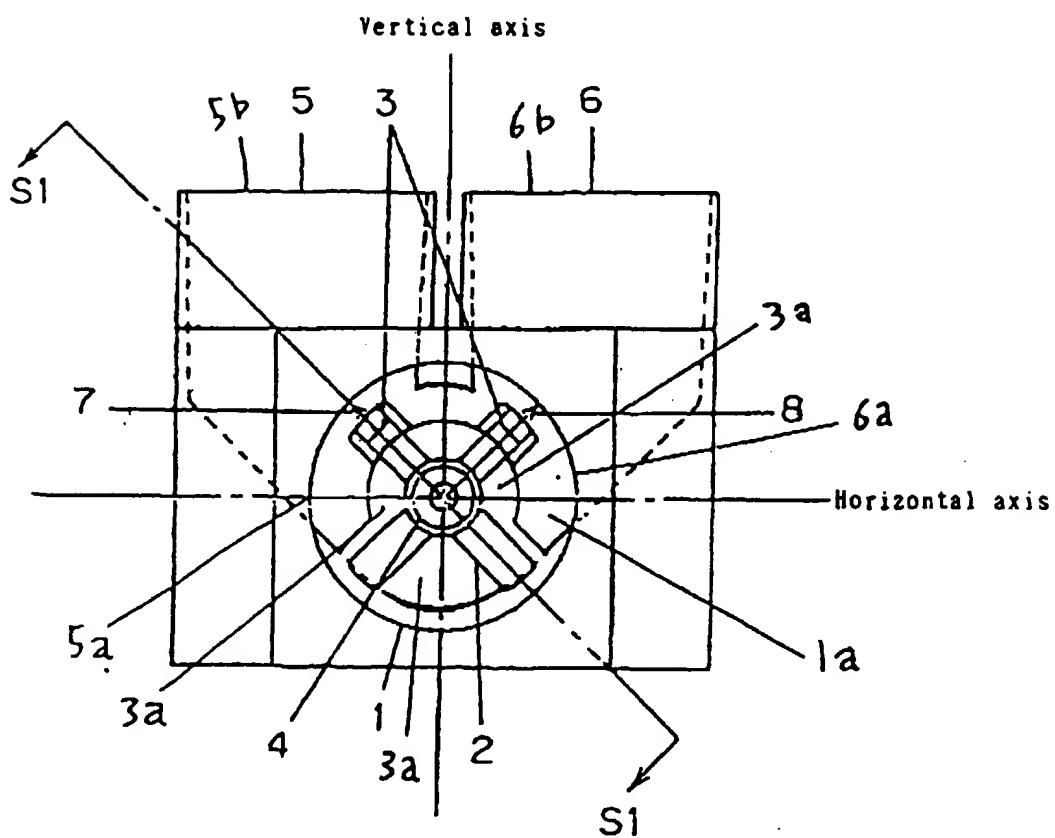


Fig. 4

- 1 Circular waveguide
- 1b Opening plane
- 2 Cross shaped branching transforming unit
- 3 Stairs
- 4 Metal columnar blocks
- 5 Rectangular waveguide for first polarized wave
- 6 Rectangular waveguide for second polarized wave
- 9 Rectangular TE<sub>11</sub> mode
- 10 Circular TE<sub>11</sub> mode

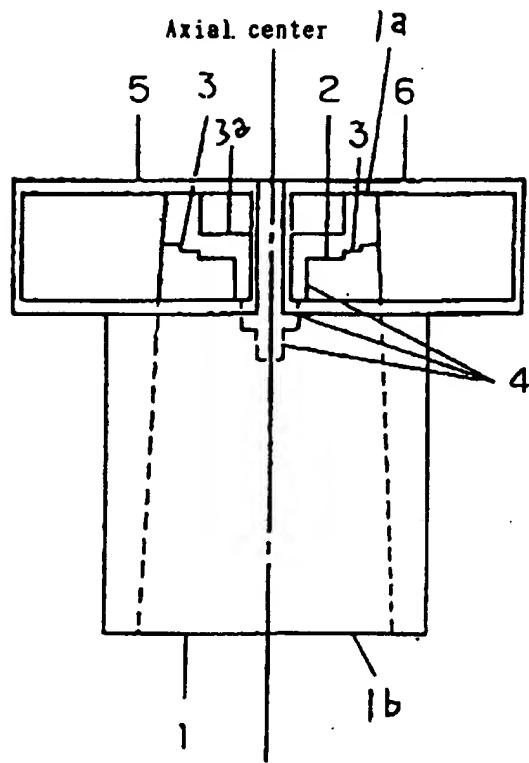
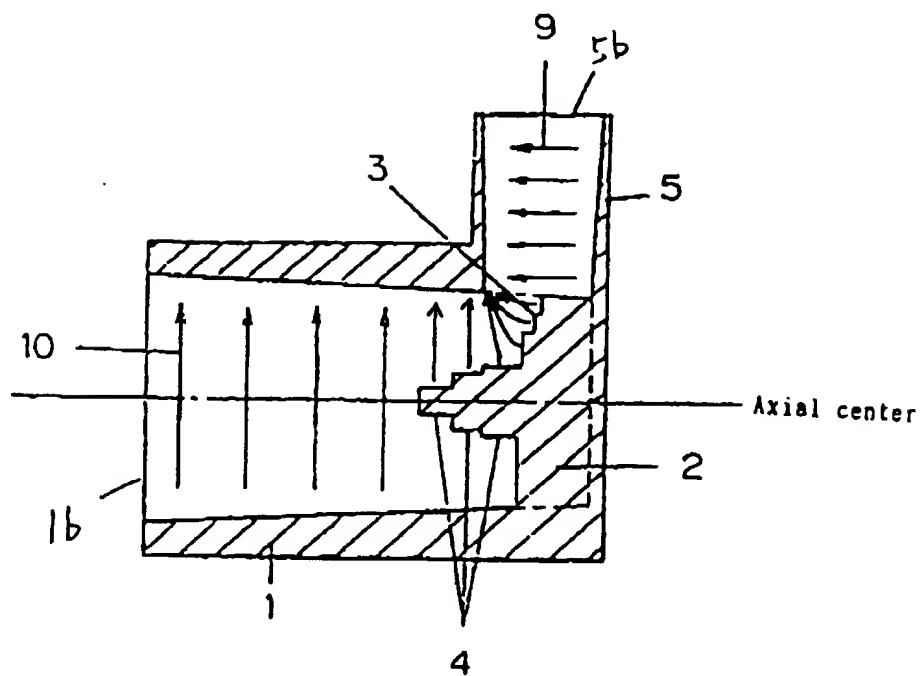


Fig. 5

- 1 Circular waveguide
- 2 Cross shaped branching transforming unit
- 3 Stairs
- 4 Metal columnar blocks
- 5 Rectangular waveguide for first polarized wave
- 9 Rectangular TE<sub>10</sub> mode
- 10 Circular TE<sub>11</sub> mode





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## EUROPEAN SEARCH REPORT

Application Number  
EP 96 30 7303

DOCUMENTS CONSIDERED TO BE RELEVANT			CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	
X	US 3 668 567 A (ROSEN) 6 June 1972 * column 3, line 39 - column 4, line 2; figures 1-4 *	1,2,5,6	H01P1/161
Y	---	3,4,7,8	
Y	GB 870 873 A (COMPAGNIE FRANCAISE THOMSON-HOUSTON) 21 June 1961 * page 1, line 70 - line 91; figure 1 *	3,4,7,8	
A	PATENT ABSTRACTS OF JAPAN vol. 17, no. 359 (E-1395), 7 July 1993 & JP 05 055807 A (FUJITSU GENERAL LTD), 5 March 1993, * abstract *	1,2,5,6	
A	PATENT ABSTRACTS OF JAPAN vol. 10, no. 213 (E-422), 25 July 1986 & JP 61 052002 A (MITSUBISHI ELECTRIC CORP), 14 March 1986, * abstract *	5	
			TECHNICAL FIELDS SEARCHED (Int.Cl.6)
			H01P
<p>The present search report has been drawn up for all claims</p>			
Place of search	Date of compilation of the search	Examiner	
THE HAGUE	17 February 1997	Den Otter, A	
CATEGORY OF CITED DOCUMENTS			
X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document			
T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document			